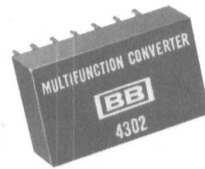


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4302

Low Cost MULTIFUNCTION CONVERTER

FEATURES

- VERSATILE
- SMALL PACKAGE: Dual-in-Line
- EASY TO USE

DESCRIPTION

Burr-Brown's multifunction converter model 4302 is a low cost solution to many analog conversion needs. Much more than just a multiplier/divider, the 4302 performs many analog circuit functions with a high degree of accuracy at a low total cost.

| FUNCTIONS | ACCURACY |
|--------------------|-----------------|
| Multiply | ±0.25% |
| Divide | ±0.25% |
| Square | ±0.03% |
| Square Root | ±0.07% |
| Exponentiate | ±0.15% (m = 5) |
| Roots | ±0.2% (m = 0.2) |
| Sine θ | ±0.5% |
| Cosine θ | ±0.8% |
| Tan $^{-1}$ (Y/X) | ±0.6% |
| $\sqrt{X^2 + Y^2}$ | ±0.07% |

Typical accuracies expressed as a % of output full scale (+10VDC) at 25°C.

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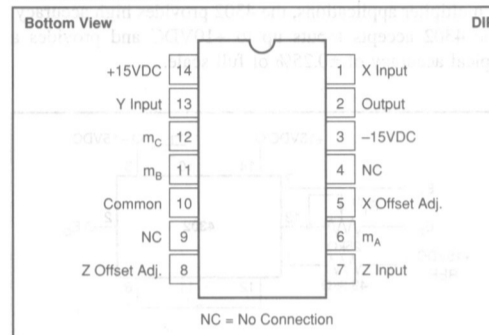
SPECIFICATIONS

ELECTRICAL

$T_A = +25^\circ\text{C}$, $V_S = \pm 15\text{VDC}$, unless otherwise noted.

| MODEL | 4302 |
|--|--|
| TRANSFER FUNCTION | $E_o = V_y \left[\frac{V_z}{V_x} \right]^m$ |
| RATED OUTPUT Voltage Current | +10.0V 5mA |
| INPUT Signal Range Absolute Maximum Impedance (X/Y/Z) | $0 \leq (V_x, V_y, V_z) \leq +10\text{V}$ $(V_x, V_y, V_z) \leq \pm 18\text{V}$ 100k Ω /90k Ω /100k Ω |
| EXPONENT RANGE Roots ($0.2 \leq m < 1$) Powers ($1 < m \leq 5$) ($m = 1$) | $m = \frac{R_2}{R_1 + R_2}$ Refer to Functional Diagram Below. $m = \frac{R_1 + R_2}{R_2}$ $R_1 = 0\Omega$, R_2 not used |
| POWER REQUIREMENTS Rated Supply Range Quiescent Current | $\pm 15\text{VDC}$ ± 12 to $\pm 18\text{VDC}$ $\pm 10\text{mA}$ |
| TEMPERATURE RANGE Operating Storage | -25°C to $+85^\circ\text{C}$ -25°C to $+85^\circ\text{C}$ |

PIN CONFIGURATION



PACKAGE INFORMATION⁽¹⁾

| MODEL | PACKAGE | PACKAGE DRAWING NUMBER |
|-------|--------------------|------------------------|
| 4302 | 14-Pin Plastic DIP | 003 |

NOTE: (1) For detailed drawing and dimension table, please see end of data sheet, or Appendix D of Burr-Brown IC Data Book.

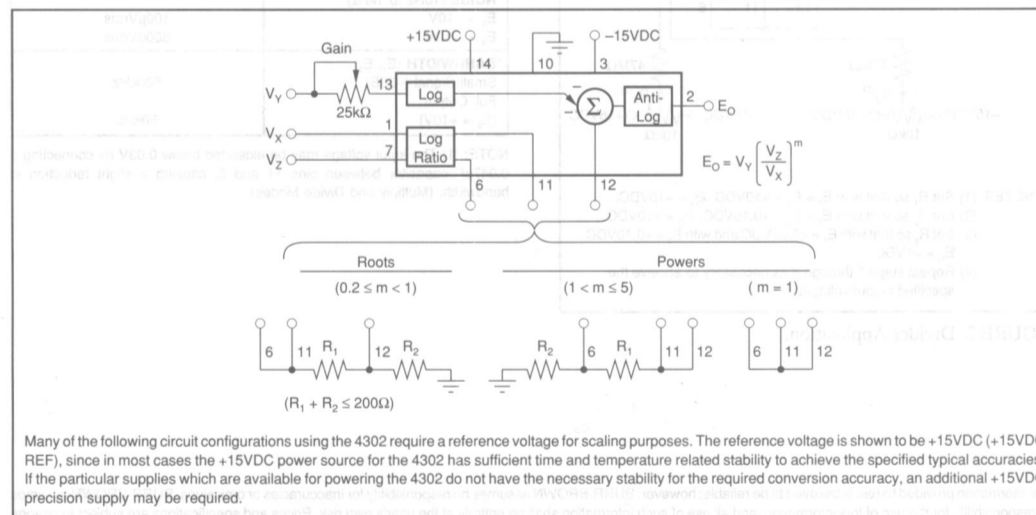
APPLICATION INFORMATION

General specifications for the 4302 multifunction converter are presented on this page. These specifications characterize the 4302 as a versatile three input multifunction converter.

The following pages are applications intended to help you apply the 4302 to your particular circuit function need. These pages contain dedicated circuit configurations in

order to produce the functions of: multiplication, division, exponentiation, square rooting, squaring, sine, cosine, arctangent, and vector algebra.

It is the purpose of this product data sheet to enable you to apply the 4302 to your analog conversion needs quickly and efficiently.



4302 Functional Diagram.

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MULTIPLIER/ DIVIDER FUNCTIONS

MULTIPLIER

In multiplier applications, the 4302 provides high accuracy. The 4302 accepts inputs up to +10VDC and provides a typical accuracy of $\pm 0.25\%$ of full scale.

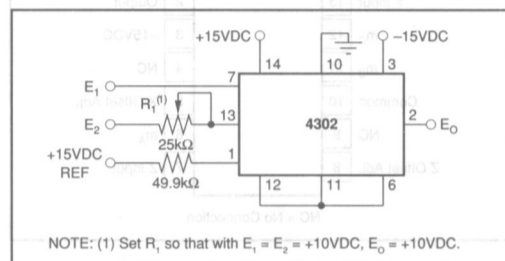


FIGURE 1. Multiplier Application.

DIVIDER

As a divider, the 4302 provides a typical conversion accuracy of $\pm 0.25\%$ of full scale.

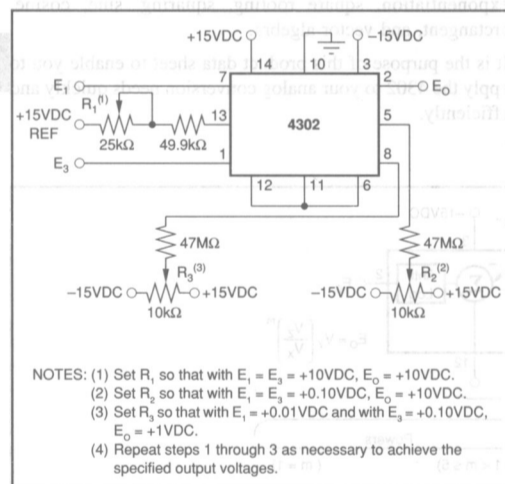


FIGURE 2. Divider Application.

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| TRANSFER FUNCTION | $E_O = + \frac{E_1 E_2}{10}$ |
|-----------------------------------|---|
| ACCURACY | |
| Total Errors | |
| Typical at +25°C | $\pm 25\text{mV}$ |
| Maximum at +25°C | $\pm 50\text{mV}$ |
| (for input range) | $0.03\text{V} \leq E_1 \leq 10\text{V}$ |
| | $0.01\text{V} \leq E_2 \leq 10\text{V}$ |
| vs Temperature | $\pm 1\text{mV}/^\circ\text{C}$ |
| Offset Errors ($E_1 = E_2 = 0$) | |
| Output Offset (at 25°C) | $\pm 10\text{mV}$ |
| vs Temperature | $\pm 0.2\text{mV}/^\circ\text{C}$ |
| NOISE (10Hz to 1kHz) | 100 μVrms |
| BANDWIDTH (E_1, E_2) | |
| Small Signal (-3dB) | 500kHz |
| Full Output | 60kHz |

NOTE: (1) The input voltage may be extended below 0.03V by connecting a 0.047 μF capacitor between pins 11 and 5, causing a slight reduction in bandwidth. (Multiply and Divide Modes).

| TRANSFER FUNCTION | $E_O = +10 (E_1/E_2)$ |
|--|---|
| ACCURACY | |
| Total Errors | |
| Typical at +25°C | $\pm 25\text{mV}$ |
| Maximum at +25°C | $\pm 50\text{mV}$ |
| (for E_1, E_2 and input range) | $0.03\text{V} \leq E_1 \leq 10\text{V}$ |
| | $0.01\text{V} \leq E_2 \leq 10\text{V}$ |
| vs Temperature | $\pm 1\text{mV}/^\circ\text{C}$ |
| Offset Errors ($E_1 = 0, E_2 = +10\text{V}$) | |
| Output Offset (at 25°C) | $\pm 10\text{mV}$ |
| vs Temperature | $\pm 1\text{mV}/^\circ\text{C}$ |
| NOISE (10Hz to 1kHz) | |
| $E_2 = +10\text{V}$ | 100 μVrms |
| $E_2 = +0.1\text{V}$ | 300 μVrms |
| BANDWIDTH (E_1, E_2) | |
| Small Signal (-3dB) | 500kHz |
| Full Output | 60kHz |

NOTE: (1) The input voltage may be extended below 0.03V by connecting a 0.047 μF capacitor between pins 11 and 5, causing a slight reduction in bandwidth. (Multiply and Divide Modes).

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EXPONENTIAL FUNCTIONS

Model 4302 may be used as exponentiator over a range of exponents from 0.2 to 5. The exponents 0.5 and 2, square rooting and squaring, respectively, are often used functions and are treated below. Other values of exponents (m) may be useful in terms of linearization of nonlinear functions or simply for producing the mathematical conversions. Characteristics of m = 0.2 and m = 5 are presented on the right. For other values of m, the curves presented in Figure 3 may be used to interpolate the error for a nonspecified value of m.

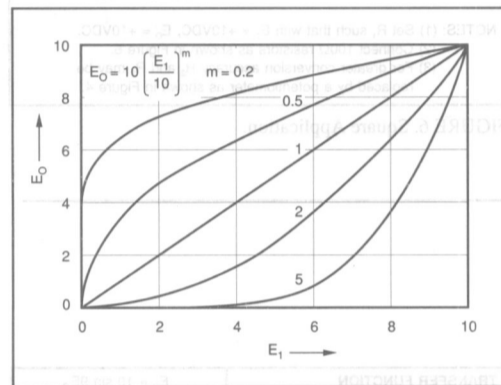
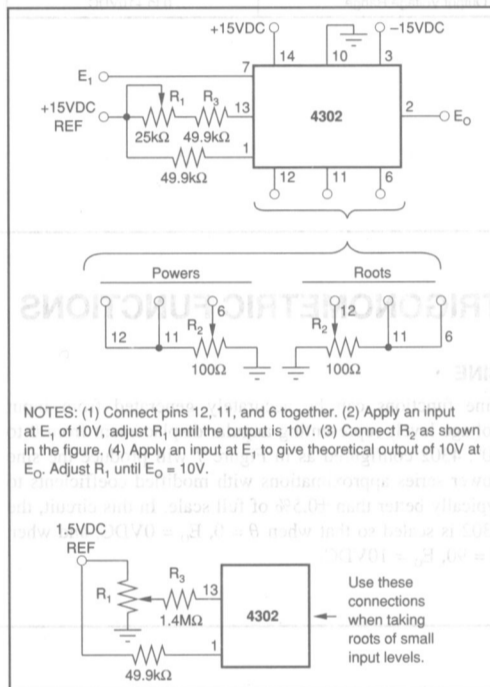


FIGURE 3. Exponentiator Transfer Characteristics.

| TRANSFER FUNCTION | $E_o = 10 \left(\frac{E_i}{10} \right)^m$ |
|----------------------------------|--|
| Total Conversion Error (typical) | |
| m = 0.2 | |
| 0.5VDC < E _i ≤ 10VDC | ±2mVDC |
| 0.1VDC < E _i ≤ 0.5VDC | ±25mVDC |
| m = 5 | |
| 1VDC < E _i ≤ 10VDC | ±15mVDC |
| Exponent Range (continuous) | 0.2 ≤ m ≤ 5 |
| Input Voltage Range | 0 to +10VDC |
| Output Voltage Range | 0 to +10VDC |



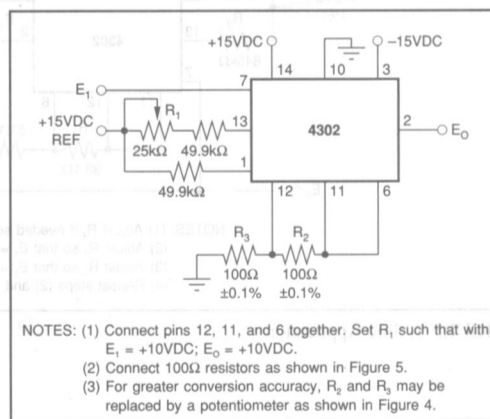
NOTES: (1) Connect pins 12, 11, and 6 together. (2) Apply an input at E_i of 10V, adjust R₁ until the output is 10V. (3) Connect R₂ as shown in the figure. (4) Apply an input at E_i to give theoretical output of 10V at E_o. Adjust R₁ until E_o = 10V.

FIGURE 4. Exponential Functions.

SQUARE ROOT

As a Square Rooter (m = 0.5), the 4302 provides a typical total conversion accuracy of ±0.07%. Refer to Figure 5 and notes for connections and adjustments, respectively.

| TRANSFER FUNCTION | $E_o = 10 \sqrt{\frac{E_i}{10}}$ |
|-----------------------------------|----------------------------------|
| Total Conversion Error (typical) | |
| 0.5VDC < E _i ≤ 10VDC | ±7mV |
| 0.02VDC < E _i ≤ 0.5VDC | ±55mV |
| Input Voltage Range | 0 to +10VDC |
| Output Voltage Range | 0 to +10VDC |



NOTES: (1) Connect pins 12, 11, and 6 together. Set R₁ such that with E_i = +10VDC; E_o = +10VDC. (2) Connect 100Ω resistors as shown in Figure 5. (3) For greater conversion accuracy, R₂ and R₃ may be replaced by a potentiometer as shown in Figure 4.

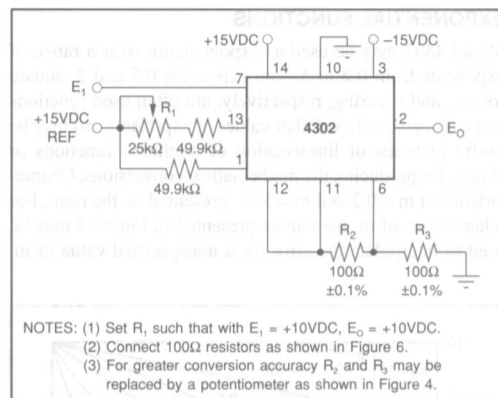
FIGURE 5. Square Root Application.

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SQUARE

Configured as a Square Function Converter ($m = 2$), the 4302 produces high conversion accuracies of typically 0.03%. Refer to Figure 6 and accompanying notes.

| | |
|--|--|
| TRANSFER FUNCTION | $E_o = 10 \left(\frac{E_i}{10} \right)^2$ |
| Total Conversion Error (typical) 0.1VDC $\leq E_i \leq$ 10VDC | $\pm 3\text{mV}$ |
| Input Voltage Range | 0 to +10VDC |
| Output Voltage Range | 0 to +10VDC |



NOTES: (1) Set R_1 such that with $E_i = +10\text{VDC}$, $E_o = +10\text{VDC}$.
(2) Connect 100Ω resistors as shown in Figure 6.
(3) For greater conversion accuracy R_2 and R_3 may be replaced by a potentiometer as shown in Figure 4.

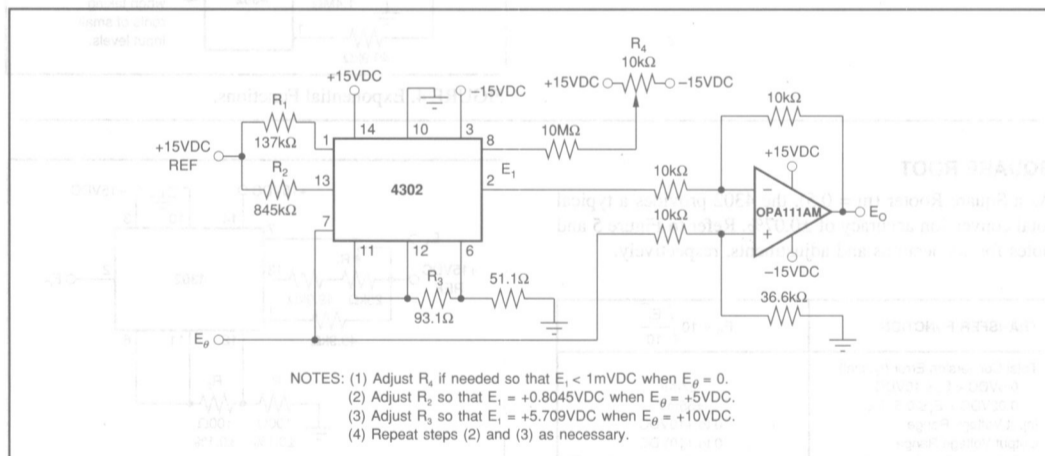
FIGURE 6. Square Application.

TRIGONOMETRIC FUNCTIONS

SINE

Sine functions can be accurately generated from input voltage levels representing angular displacement from 0 to 90°. 4302 configured as in Figure 7 will produce the sine power series approximations with modified coefficients to typically better than $\pm 0.5\%$ of full scale. In this circuit, the 4302 is scaled so that when $\theta = 0$, $E_o = 0\text{VDC}$, and when $\theta = 90$, $E_o = 10\text{VDC}$.

| | |
|---|---|
| TRANSFER FUNCTION | $E_o = 10 \sin 9E_\theta$ |
| Power Series Approximation | $E_o = 1.5708E_\theta - 1.5924 \left(\frac{E_\theta}{6.366} \right)^{2.827}$ |
| Total Conversion Error (typical) | $\pm 50\text{mV}$ |
| Input Voltage Range ($0 \leq \theta \leq 90^\circ$) | 0 to +10VDC |
| Output Voltage Range ($0 \leq \sin \theta \leq 1$) | 0 to +10VDC |



NOTES: (1) Adjust R_1 if needed so that $E_i < 1\text{mVDC}$ when $E_\theta = 0$.
(2) Adjust R_2 so that $E_i = +0.8045\text{VDC}$ when $E_\theta = +5\text{VDC}$.
(3) Adjust R_3 so that $E_i = +5.709\text{VDC}$ when $E_\theta = +10\text{VDC}$.
(4) Repeat steps (2) and (3) as necessary.

FIGURE 7. Sine Application.

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COSINE

Connected as in Figure 2, 4302 will generate a cosine function of the input voltage. Typical accuracies of $\pm 0.8\%$ can be expected from this configuration.

| | |
|---|--|
| TRANSFER FUNCTION | $E_o = 10 \cos 9E_\theta$ |
| Power Series Approximation | $E_o = 10 + 0.3652 E_\theta - 0.4276 E_\theta^{1.504}$ |
| Total Conversion Error (typical) | $\pm 80\text{mV}$ |
| Input Voltage Range ($0 \leq \theta \leq 90^\circ$) | 0VDC to +10VDC |
| Output Voltage Range ($1 \leq \cos \theta \leq 0$) | +10VDC to 0VDC |

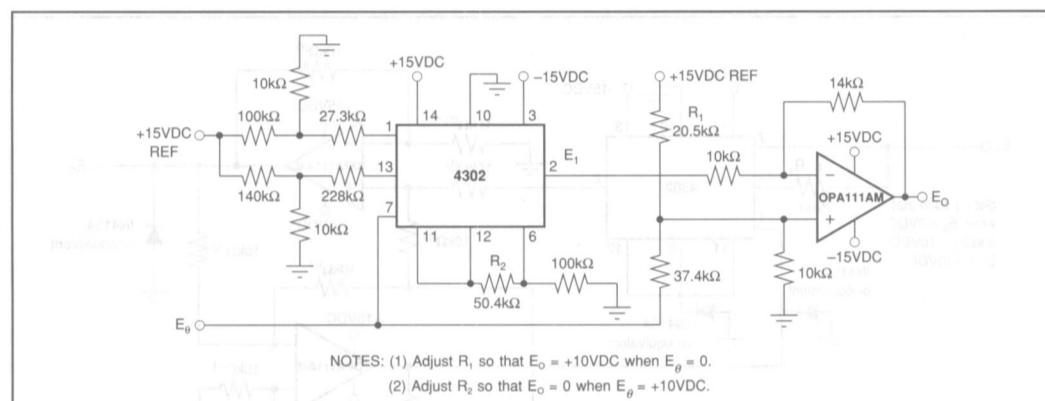


FIGURE 8. Cosine Application.

ARCTANGENT

4302 and the associated circuitry shown below will produce the inverse tangent of a ratio. This application is particularly well suited to conversion from rectangular coordinates to polar coordinates where

$$E_\theta = \tan^{-1} \frac{E_y}{E_x}$$

The accuracy of conversion depends upon the levels of the input signals. Refer to table at right.

| | |
|--|--|
| TRANSFER FUNCTION | $E_o = \tan^{-1} \left(\frac{[E_1]}{[E_2]} \right)$ |
| Power Series Approximation | $E_o = \frac{\left(\frac{[E_1]}{[E_2]} \right)^{1.2125}}{1 + \left(\frac{[E_1]}{[E_2]} \right)^{1.2125}} (90^\circ)$ |
| Total Conversion Error | $\pm 55\text{mVDC}$ |
| $2 < E_1, E_2 \leq 10\text{VDC}$ | $\pm 65\text{mVDC}$ |
| $0.1 < E_1, E_2 \leq 2\text{VDC}$ | $\pm 340\text{mVDC}$ |
| $0.03 < E_1, E_2 \leq 0.1\text{VDC}$ | +0.01VDC to +10VDC |
| Input Voltage Range (E_1, E_2) | 0VDC to +9VDC |
| Output Voltage Range $0 \leq E_\theta \leq 90^\circ$ | |

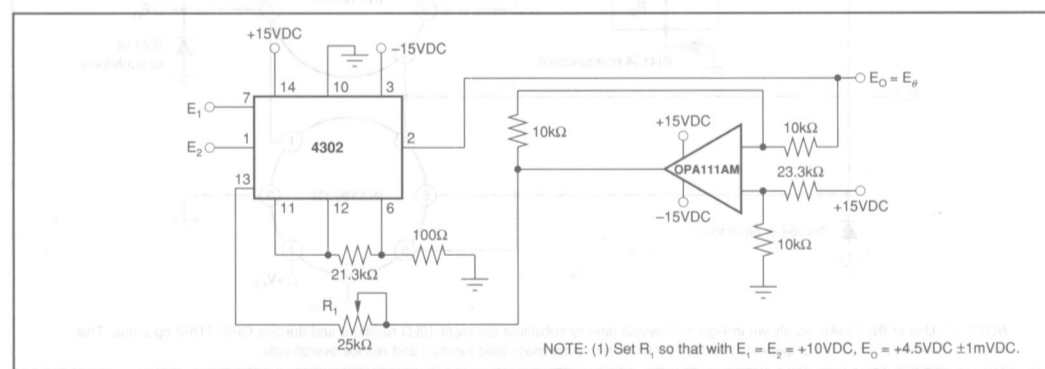


FIGURE 9. Arctangent Application.

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VECTOR MAGNITUDE FUNCTION

The 4302 will produce the square root of the sum of the squares of two inputs. This function is companion to the arctangent of a ratio for the conversion of rectangular to polar coordinates.

| TRANSFER FUNCTION | $E_o = \sqrt{E_1^2 + E_2^2}$ |
|--|---------------------------------|
| Input Voltage Range E_1 E_2 (refer to notes 1 and 2) | 0 to +10VDC -10VDC to +10VDC |
| Output Voltage Range | 0 to +10VDC |
| Conversion Error | $\pm 7\text{mVDC}$ |

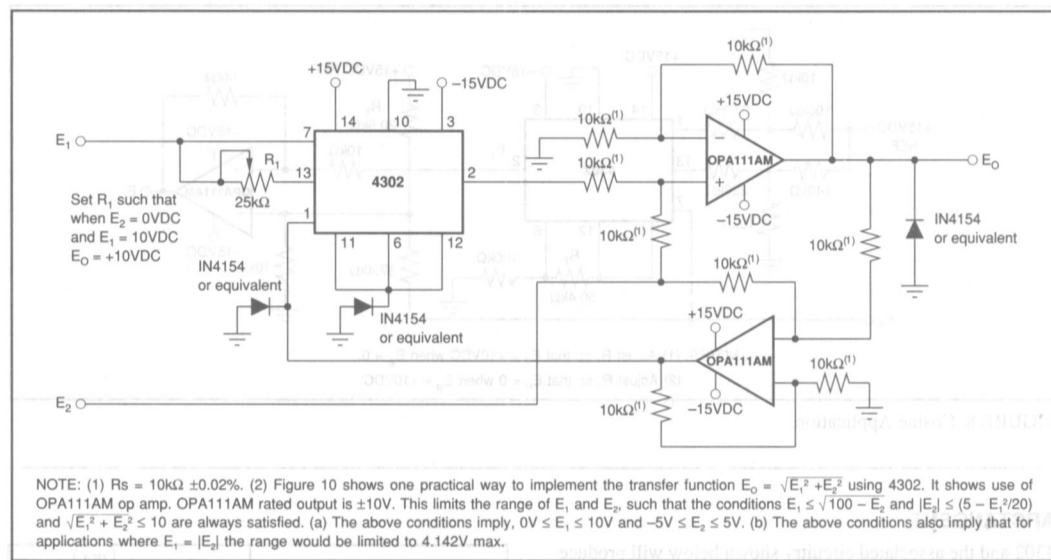


FIGURE 10. Implementation of Transfer Function.

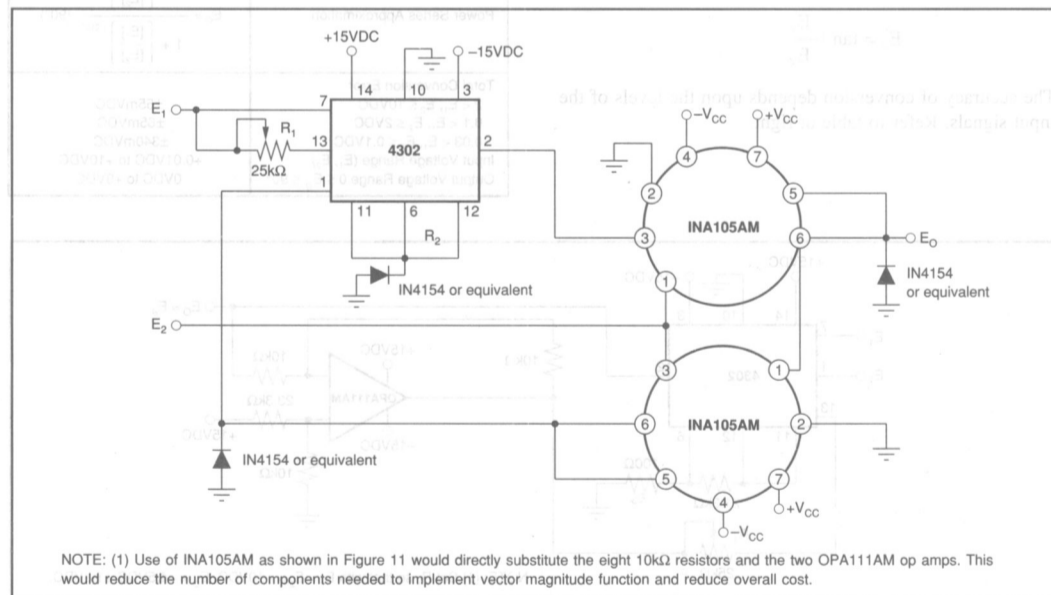


FIGURE 11. Vector Magnitude Function Application.



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4341

Low Cost TRUE RMS-TO-DC CONVERTER

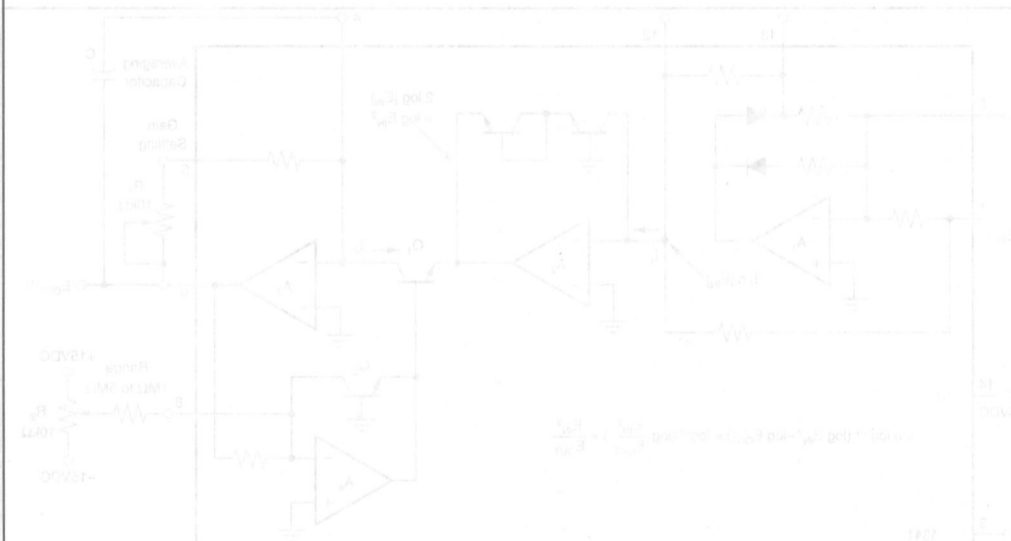
FEATURES

- LOW COST
- HIGH ACCURACY: $\pm 0.2\%$ $\pm 2mV$
- VERSATILE: AC and DC Inputs

DESCRIPTION

The 4341 RMS-to-DC converter features low cost without sacrificing performance. The 4341 computes a DC voltage proportional to the true rms value of signals which may be complex waveforms, DC levels, or a combination of both.

The input and output are fully protected against over-voltages and short circuits. Provisions for the external adjustment of gain, offset voltage, DC-reversal error, and frequency response make the 4341 versatile enough to fill the majority of your applications.



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PDS-323B

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4341
7
SPECIAL FUNCTIONS

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SPECIFICATIONS

ELECTRICAL

$T_A = +25^\circ\text{C}$, $V_S = \pm 15\text{VDC}$, unless otherwise noted.

| PARAMETER | CONDITIONS |
|------------------------------------|---|
| TRANSFER FUNCTION | $E_{\text{rms}}(t) = \sqrt{\frac{1}{T} \int_0^T [E_{\text{IN}}(t)]^2 dt}$ |
| INPUT | |
| Peak Operating Voltage | $\pm 10\text{V}$ |
| Absolute Maximum Voltage | $\pm \text{Supply}$ |
| Impedance | $5\text{k}\Omega$ |
| OUTPUT | |
| Voltage | 0 to $+10\text{V}$ |
| Current | $+5\text{mA}$, min |
| Resistance | 1Ω , max |
| BANDWIDTH | |
| $\pm 1\%$ of Theoretical Output | 80kHz |
| -3dB | 450kHz |
| CONVERSION ACCURACY ⁽¹⁾ | |
| Input: 500mVrms to 5.0Vrms | $\pm 0.5\%$ of Reading, max ⁽¹⁾ |
| Input: DC to 10kHz Sine Wave | |
| Input: 10mVrms to 7Vrms | |
| Input: DC to 20kHz | $\pm 2\text{mV} \pm 0.2\%$ of Reading |
| STABILITY | |
| Accuracy vs Temperature | $\pm 0.1\text{mV} \pm 0.01\%$ of Reading/ $^\circ\text{C}$ |
| Accuracy vs Supply Voltage | $\pm 0.1\text{mV} \pm 0.01\%$ of Reading/ $\%$ of Supply Voltage Change |
| TEMPERATURE RANGE | |
| Operating | -25°C to $+85^\circ\text{C}$ |
| Storage | -40°C to $+85^\circ\text{C}$ |
| POWER REQUIREMENTS | |
| Rated Voltage | $\pm 15\text{VDC}$ |
| Voltage Range | $\pm 14\text{VDC}$ to $\pm 16\text{VDC}$ |
| Quiescent Current | $\pm 12\text{mA}$, typ, $\pm 24\text{mA}$, max |

NOTES: (1) After standard trim procedure (see below). (2) Model 4341 will convert DC inputs. Lower frequency AC inputs require a large value of averaging capacitor to minimize ripple at output. (see Figure 2).

STANDARD TRIM PROCEDURE

If the 4341 is used to measure sine waves or distorted sine waves, only two trims are needed to achieve an accuracy of $\pm 0.5\%$ of reading from 500mVrms to 5Vrms up to 10kHz. Refer to Figure 1.

1. Set $E_{\text{IN}} = 5.000\text{Vrms} \pm 0.02\%$ and adjust R_1 such that $E_{\text{O}} = 5.000\text{VDC} \pm 2\text{mV}$.
2. Set $E_{\text{IN}} = 500\text{mVrms} \pm 0.02\%$ and adjust R_2 such that $E_{\text{O}} = 500\text{mVDC} \pm 0.2\text{mV}$.
3. Repeat Step 1.

THEORY OF OPERATION

The true rms value of a time-varying signal $E(t)$ over a time period T is

$$E_{\text{rms}}(t) = \sqrt{\frac{1}{T} \int_0^T [E_{\text{IN}}(t)]^2 dt}$$

The required operations are squaring, averaging and square rooting. A simplified schematic diagram of the 4341 is shown in Figure 1. The A_1 circuit produces a current, i_1 , which is proportional to the rectified input voltage. The A_2 circuit is a logarithmic amplifier which produces a voltage proportional to $2 \log E_{\text{IN}}$ or $\log E_{\text{IN}}^2$. The logarithmic gain of the A_2 circuit is derived from the inherent exponential characteristics of transistor junctions. By using proprietary

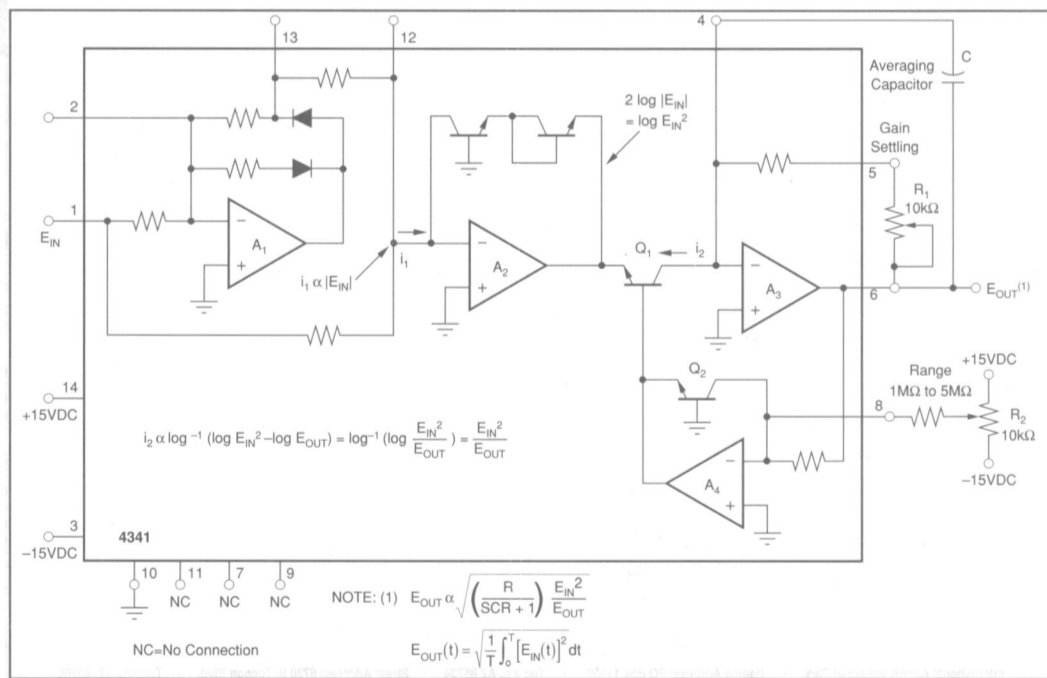


FIGURE 1. Simplified Schematic.

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monolithic components, the circuit provides an accurate log function over many decades which is relatively insensitive to temperature variations. Amplifier A_4 uses the same techniques as A_2 to generate $\log E_{OUT}$.

Transistor Q_1 produces a collector current, i_2 , proportional to the antilog of its base-emitter voltage such that

$$i_2 \propto \log^{-1}(\log E_{IN}^2 - \log E_{OUT})$$

$$= \log^{-1}(\log E_{IN}^2 / E_{OUT}) = E_{IN}^2 / E_{OUT}$$

The A_3 circuit, which contains the external capacitor, takes the time average of the i_2 signal and produces E_{OUT} , which is directly proportional to the rms value of E_{IN} .

Figures 2 and 3 show the effects of the external filter capacitor on ripple magnitude and response time. As the frequency of the input approaches DC, the 4341 begins to act like a full wave rectifier such that the output is the absolute value of the input. While the 4341 will accurately convert DC input voltages, the averaging capacitor must be made very large to minimize ripple at low frequencies.

CHOOSING THE AVERAGING CAPACITOR

A single-pole low-pass RC filter provides the averaging function. The time constant is $1/2 RC$ where R is $10k\Omega$ when the 4341 is adjusted for unity gain. To select the best value of C , make a tradeoff between output ripple and response time. Figure 2 shows the ripple magnitude vs frequency for several typical values of capacitor. Response time vs capacitor value is shown in Figure 3. (Note that rise times and fall times are different for the same value of capacitor).

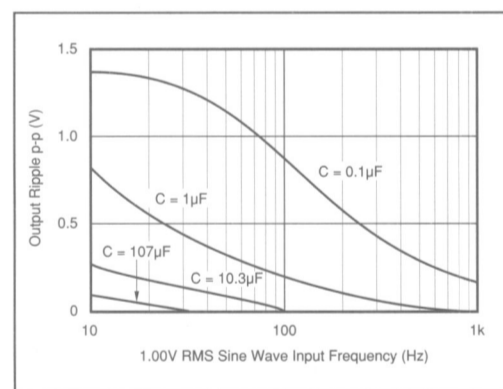


FIGURE 2. Output Ripple Magnitude vs Input Signal Frequency.

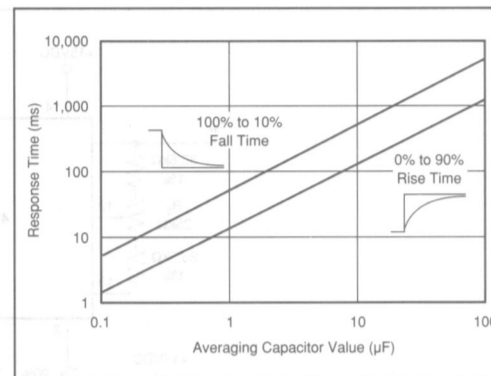


FIGURE 3. Response Time vs Value of Averaging Capacitor.

While the ripple magnitude for signals other than sine waves can be analytically determined, it is tedious. The fastest method of choosing C is to apply a representative input signal and observe the output for various values of C . C can be 100s of microfarads, but should have a leakage current less than $0.1\mu A$ to minimize gain errors. With very large values of C , the input signals with frequencies approaching DC level could be averaged. Since the output is always a positive voltage, C can be a polar capacitor.

EXPANDED TRIM PROCEDURE FOR GREATER ACCURACY

If the 4341 is used in applications to measure complex waveforms, the following expanded trim procedure is recommended. (Refer to Figure 4).

First, set all potentiometers at mid turn position.

1. DC Reversal Error — Apply $+10.000V \pm 1mV$ and $-10.000V \pm 1mV$ to E_{IN} alternatively, adjust R_3 such that E_o readings are the same $\pm 2mV$.
2. Gain Adjustment — Apply $E_{IN} = +10.000VDC \pm 1mV$, adjust R_1 such that $E_o = +10.000VDC \pm 1mV$.
3. Input Offset — Apply $+10.0mV \pm 0.1mV$ and $-10.0mV \pm 0.1mV$ to E_{IN} , adjust R_4 such that E_o readings are the same $\pm 0.1mV$.
4. Offset — Ground E_{IN} , adjust R_3 such that $E_o = 0 \pm 0.1mV$. Repeat Step (3).
5. Low Level Accuracy — Apply $E_{IN} = +10.0mV \pm 0.1mV$, adjust R_2 such that $E_o = +10.0mV \pm 0.1mV$.

NONUNITY GAINS

Gain values greater than unity can be achieved by inserting resistor R_x between pin 5 and pin 6. $R_x = (A^2 - 1) \times 10k + 2k$ where A is the desired value of gain ($1 < A \leq 10$). (R_x is in Ω).

4341

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SPECIAL FUNCTIONS

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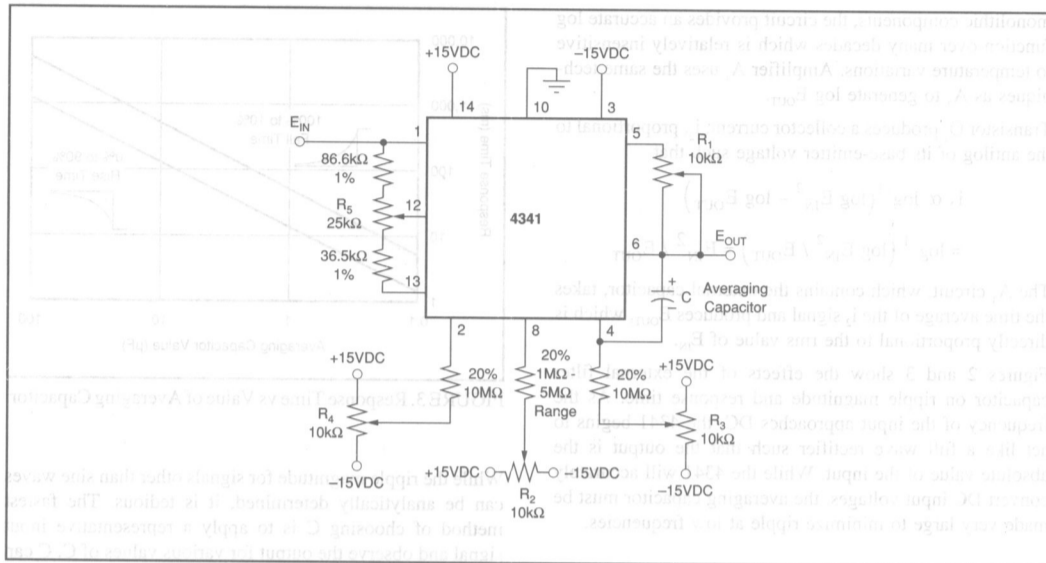


FIGURE 4. Expanded Trim Procedure (High Accuracy Applications).

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EXPANDED TRIM PROCEDURE FOR GREATER ACCURACY

1. DC Relevel Error — Apply $E_{IN} = +10.000V$ and $-10.000V$ to E_{IN} alternately. Adjust R_1 such that E_{OUT} readings are the same $±0.01V$.
2. Gain Adjustment — Apply $E_{IN} = +10.000V$ and $-10.000V$ to E_{IN} alternately. Adjust R_2 such that E_{OUT} readings are the same $±0.01V$.
3. Input Offset — Apply $E_{IN} = +10.000V$ and $-10.000V$ to E_{IN} alternately. Adjust R_3 such that E_{OUT} readings are the same $±0.01V$.
4. Offset — Ground E_{IN} . Adjust R_4 such that $E_{OUT} = 0.00V$.
5. Low Level Accuracy — Apply $E_{IN} = +10.000V$ and $-10.000V$ to E_{IN} alternately. Adjust R_5 such that E_{OUT} readings are the same $±0.01V$.

NONUNITY GAINS

Gain values greater than unity can be achieved by increasing the feedback resistor R_2 between pins 2 and 6. $A_v = 1 + R_2/R_1$ where A_v is the desired value of gain ($A_v < 10^4$) and R_1 is the feedback resistor value.

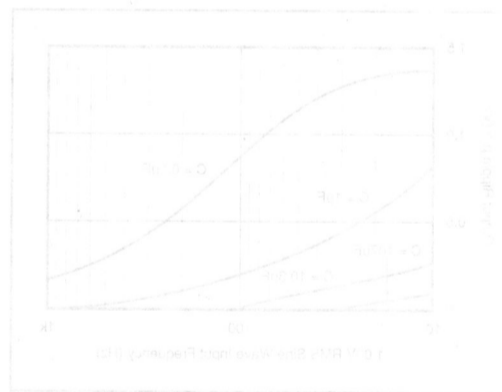


FIGURE 5. Output Signal Magnitude vs. Input Signal for Various Gain Settings.